A Hybrid Second Moment Method for Thermal Radiative Transfer M&C 2025

M. Pozulp^{1,3}, T. Haut¹, P. Brantley¹, S. Olivier², J. Vujic³

¹Lawrence Livermore National Laboratory ²Los Alamos National Laboratory ³University of California, Berkeley

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Hybrid Second Moment Method Numerical Results Noisy Crooked Pipe







Hybrid Second Moment Method Numerical Results **Noisy Crooked Pipe** Variance Reduction







Hybrid Second Moment Method Numerical Results **Noisy Crooked Pipe** Variance Reduction Incorrect Crooked Pipe







Hybrid Second Moment Method Numerical Results **Noisy Crooked Pipe** Variance Reduction Incorrect Crooked Pipe Correct Crooked Pipe Conclusion



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Hybrid Second Moment (HSM) solves a linear transport equation.

$$\mathbf{\Omega} \cdot \nabla \psi + \sigma_t \psi = \frac{\sigma_s}{4\pi} \int_{\mathbb{S}^2} \psi \, \mathrm{d}\Omega' + q$$





$$\boldsymbol{\Omega} \cdot \nabla \psi + \sigma_t \psi = \frac{\sigma_s}{4\pi} \int_{\mathbb{S}^2} \psi \, \mathrm{d}\Omega' + q \,,$$
 (1a)

$$\psi(\mathbf{x}, \boldsymbol{\Omega}) = \psi_{\mathsf{inc}}(\mathbf{x}, \boldsymbol{\Omega}) \,, \quad \mathbf{x} \in \partial \mathcal{D} \text{ and } \boldsymbol{\Omega} \cdot \mathbf{n} < 0 \,.$$
 (1b)





This system is an equivalent reformulation of eqs. (1a) and (1b).

$$\nabla \cdot \boldsymbol{J} + \sigma_a \varphi = Q_0, \quad \mathbf{x} \in \mathcal{D},$$
(2a)
$$\frac{1}{3} \nabla \varphi + \sigma_t \boldsymbol{J} = \boldsymbol{Q}_1 - \nabla \cdot \mathbf{T}, \quad \mathbf{x} \in \mathcal{D}.$$
(2b)
$$\boldsymbol{J} \cdot \mathbf{n} = \frac{1}{2} \varphi + 2J_{\text{in}} + \beta, \quad \mathbf{x} \in \partial \mathcal{D}.$$
(2c)





$$egin{aligned} & \mathbf{\Omega}\cdot
abla \psi + \sigma_t \psi = \overline{rac{\sigma_s}{4\pi}} arphi + q\,, \ & \psi(\mathbf{x}, \mathbf{\Omega}) = ar{\psi}(\mathbf{x}, \mathbf{\Omega})\,, \quad \mathbf{x} \in \partial \mathcal{D} ext{ and } \mathbf{\Omega} \cdot \mathbf{n} < 0\,. \end{aligned}$$









$$\begin{split} \mathbf{\Omega} \cdot \nabla \psi + \sigma_t \psi &= \frac{\sigma_s}{4\pi} \varphi + q \,, \\ \psi(\mathbf{x}, \mathbf{\Omega}) &= \bar{\psi}(\mathbf{x}, \mathbf{\Omega}) \,, \quad \mathbf{x} \in \partial \mathcal{D} \text{ and } \mathbf{\Omega} \cdot \mathbf{n} < 0 \,. \\ \mathbf{\nabla} \cdot \mathbf{J} + \sigma_a \varphi &= Q_0 \,, \quad \mathbf{x} \in \mathcal{D} \,, \\ \frac{1}{3} \nabla \varphi + \sigma_t \mathbf{J} &= \mathbf{Q}_1 - \nabla \cdot \mathbf{T} \,, \quad \mathbf{x} \in \mathcal{D} \,, \\ \mathbf{J} \cdot \mathbf{n} &= \frac{1}{2} \varphi + 2J_{\text{in}} + \beta \,, \quad \mathbf{x} \in \partial \mathcal{D} \,. \\ \mathbf{T}(\psi) &= \int_{\mathbb{S}^2} \mathbf{\Omega} \otimes \mathbf{\Omega} \,\psi \, \mathrm{d}\Omega - \frac{1}{3} \mathbf{I} \int_{\mathbb{S}^2} \psi \, \mathrm{d}\Omega \\ \beta(\psi) &= \int_{\mathbb{S}^2} |\mathbf{\Omega} \cdot \mathbf{n}| \,\psi \, \mathrm{d}\Omega - \frac{1}{2} \int_{\mathbb{S}^2} \psi \, \mathrm{d}\Omega \end{split}$$





We iterate to converge the scattering source.







The Crooked Pipe is commonly used for comparing methods.



thin

thick





We use a mesh of squares of equal size.





 $224 \times 128 = 28,672$





The horizontal symmetry of CP allows top/bottom plots.







Our method is much more noisy than unaccelerated Monte Carlo.







Hybrid Second Moment Method Numerical Results Noisy Crooked Pipe Variance Reduction Incorrect Crooked Pipe Correct Crooked Pipe Conclusion





The thick diffusion limit is when $\epsilon \in (0, 1] \rightarrow 0$.

$$\sigma_t = 1/\epsilon \,, \tag{3a}$$

$$\sigma_a = \epsilon \,, \tag{3b}$$

$$\sigma_s = \sigma_t - \sigma_a \,, \tag{3c}$$

$$q = \epsilon$$
. (3d)





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Theorem

Let
$$Q = \frac{\sigma_s}{4\pi} \varphi + q$$
 such that,
 $\mathbf{\Omega} \cdot \nabla \psi + \sigma_t \psi = Q$.
Then $\operatorname{Var}[\cdot]$ is,
 $(\operatorname{order}(Q))^2 \epsilon$.





Substitute
$$\psi = \frac{\varphi}{4\pi} + \tilde{\psi}$$
 into:
 $\mathbf{\Omega} \cdot \nabla \psi + \sigma_t \psi = \frac{\sigma_s}{4\pi} \varphi + q$,

to get,

$$\mathbf{\Omega} \cdot \nabla \tilde{\psi} + \sigma_t \tilde{\psi} = -\frac{1}{4\pi} (\sigma_a \varphi + \mathbf{\Omega} \cdot \nabla \varphi) + q.$$
(4)





The new solution is incorrect on material interfaces.







Before, we substituted $\psi = \frac{\varphi}{4\pi} + \tilde{\psi}$ to get:

$$\mathbf{\Omega} \cdot \nabla \tilde{\psi} + \sigma_t \tilde{\psi} = -\frac{1}{4\pi} (\sigma_a \varphi + \mathbf{\Omega} \cdot \nabla \varphi) + q \,.$$

Now, substitute $\psi = \frac{\bar{\varphi}}{4\pi} + \tilde{\psi}$ to get:

$$\mathbf{\Omega} \cdot \nabla \tilde{\psi} + \sigma_t \tilde{\psi} = \frac{\sigma_t}{4\pi} (\varphi - \bar{\varphi}) - \frac{1}{4\pi} (\sigma_a \varphi + \mathbf{\Omega} \cdot \nabla \bar{\varphi}) + q.$$
 (5)





Requirements:

1. $\nabla\bar{\varphi}$ is well-defined

2.
$$\varphi - \bar{\varphi}$$
 is $O(1/\sigma_t)$





Solve a transient heat conduction equation for $\bar{\varphi}$.

Requirements:

$$\frac{\partial \bar{\varphi}}{\partial t} = \nabla \cdot \frac{1}{\sigma_t} \nabla \bar{\varphi}, \quad \mathbf{x} \in \mathcal{D}, \quad \mathbf{(6)}$$

1. $\nabla \bar{\varphi}$ is well-defined

2. $\varphi - \overline{\varphi}$ is $O(1/\sigma_t)$

Take one timestep,

$$\frac{\Delta t}{h^2} \frac{1}{\max_{\mathbf{x}} \sigma_t} \ll 1.$$
 (7)



The solution on material interfaces is no longer incorrect.







The noise is gone, and the solution is not incorrect.











Runtime HSM 0m 22s UMC 41m 35s





	Runtime	Variance	FOM
HSM	0m 22s	$3.66\cdot 10^{-4}$	<mark>124.2</mark>
UMC	41m 35s	$5.20\cdot 10^{-5}$	7.7





Hybrid Second Moment Method Numerical Results **Noisy Crooked Pipe** Variance Reduction **Incorrect Crooked Pipe Correct Crooked Pipe** Conclusion





	HSM	DDMC
Orders of magnitude speedups	\checkmark	\checkmark
No diffusion approximation	\checkmark	\times
No phase-space partitioning	\checkmark	×
No issues with unstructured meshes	\checkmark	×
No iteration	×	\checkmark
No linear solver	\times	\checkmark
No negative energy-weight	\times	\checkmark
Demonstrated in production calculations	×	\checkmark



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Extra slides.





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We describe a new hybrid method that did not immediately work.

Motivation Prior Work Hybrid Second Moment Method Deterministic Component of HSM Monte Carlo Component of HSM Numerical Results Method of Manufactured Solutions Verification **Noisy Crooked Pipe** Variance Reduction Difference Formulation

Incorrect Crooked Pipe

Generalized Difference Formulation

Correct Crooked Pipe

Conclusion







- Why Monte Carlo?
- Why IMC?
- Why <u>not</u> RW?
- Why not DDMC?
- Why not Cooper, Lam, Novellino, Park, Pasmann, Willert, or any other hybrid methods?

Progress Porting LLNL Monte Carlo Transport Codes to the AMD Instict MI300A APU at 1:25 PM today in Special Session on GPU Computing



IInl.gov/article/52336/IInl-dedicates-el-capitan-ushering-new-era-

supercomputing-national-security





Hybrid Second Moment (HSM) solves a linear transport equation.

$$\boldsymbol{\Omega} \cdot \nabla \psi + \sigma_t \psi = \frac{\sigma_s}{4\pi} \int_{\mathbb{S}^2} \psi \, \mathrm{d}\Omega' + q \,, \tag{8a}$$
$$\psi(\mathbf{x}, \boldsymbol{\Omega}) = \psi_{\mathsf{inc}}(\mathbf{x}, \boldsymbol{\Omega}) \,, \quad \mathbf{x} \in \partial \mathcal{D} \text{ and } \boldsymbol{\Omega} \cdot \mathbf{n} < 0 \,. \tag{8b}$$





This system is an equivalent reformulation of eqs. (8a) and (8b).

$$abla \cdot \boldsymbol{J} + \sigma_a \varphi = Q_0, \quad \mathbf{x} \in \mathcal{D} \,,$$
(9a)

$$\frac{1}{3}\nabla\varphi + \sigma_t \boldsymbol{J} = \boldsymbol{Q}_1 - \nabla \cdot \mathbf{T}, \quad \mathbf{x} \in \mathcal{D}.$$
(9b)
$$\boldsymbol{J} \cdot \mathbf{n} = \frac{1}{2}\varphi + 2J_{\text{in}} + \beta, \quad \mathbf{x} \in \partial \mathcal{D}.$$
(9c)




The Second Moment Method iterates the scattering source.

$$\begin{split} \varphi \\ \mathbf{\Omega} \cdot \nabla \psi + \sigma_t \psi &= \frac{\sigma_s}{4\pi} \varphi + q , \\ \psi(\mathbf{x}, \mathbf{\Omega}) &= \bar{\psi}(\mathbf{x}, \mathbf{\Omega}) , \quad \mathbf{x} \in \partial \mathcal{D} \text{ and } \mathbf{\Omega} \cdot \mathbf{n} < 0 . \\ \mathbf{D} &= \int_{\mathbb{S}^2} \mathbf{\Omega} \otimes \mathbf{\Omega} \psi \, \mathrm{d} \mathbf{\Omega} - \frac{1}{3} \mathbf{I} \int_{\mathbb{S}^2} \psi \, \mathrm{d} \mathbf{\Omega} \\ \beta(\psi) &= \int_{\mathbb{S}^2} |\mathbf{\Omega} \cdot \mathbf{n}| \psi \, \mathrm{d} \mathbf{\Omega} - \frac{1}{2} \int_{\mathbb{S}^2} \psi \, \mathrm{d} \mathbf{\Omega} \end{split}$$





Find $(\varphi, \boldsymbol{J}) \in Y_p \times RT_p$ such that,

$$\int u \,\nabla \cdot \boldsymbol{J} \,\mathrm{d}\mathbf{x} + \int \sigma_a \, u\varphi \,\mathrm{d}\mathbf{x} = \int u \,Q_0 \,\mathrm{d}\mathbf{x} \,, \quad \forall u \in Y_p \,, \tag{10a}$$
$$-\frac{1}{3} \int \nabla \cdot \boldsymbol{v} \,\varphi \,\mathrm{d}\mathbf{x} + \int \sigma_t \,\boldsymbol{v} \cdot \boldsymbol{J} \,\mathrm{d}\mathbf{x} + \frac{2}{3} \int_{\Gamma_b} (\boldsymbol{v} \cdot \mathbf{n}) (\boldsymbol{J} \cdot \mathbf{n}) \,\mathrm{d}s = \int \boldsymbol{v} \cdot \boldsymbol{Q}_1 \,\mathrm{d}\mathbf{x} - \int_{\Gamma_b} \boldsymbol{v} \cdot \mathbf{Tn} \,\mathrm{d}s + \frac{2}{3} \int_{\Gamma_b} (\boldsymbol{v} \cdot \mathbf{n}) (2J_{\text{in}} + \beta) \,\mathrm{d}s - \int_{\Gamma_0} \left[v \right] \cdot \{\!\!\{\mathbf{Tn}\}\!\!\} \,\mathrm{d}s + \int \nabla_h \boldsymbol{v} : \mathbf{T} \,\mathrm{d}\mathbf{x} \quad \forall \boldsymbol{v} \in RT_p \,. \tag{10b}$$





The Monte Carlo component of HSM has no scattering events.

Estimate
$$\hat{\mathbf{T}} = \hat{\mathbf{P}} - \frac{1}{3}\mathbf{I}\hat{\phi}$$
 and $\hat{\beta} = \hat{B} - \frac{1}{2}\hat{\phi}_s$ using:
 $\hat{\phi} = \frac{1}{V}\sum_i d_i w_i, \qquad \hat{\mathbf{P}} = \frac{1}{V}\sum_i \mathbf{\Omega}_i \otimes \mathbf{\Omega}_i d_i w_i, \qquad (11a)$

$$\hat{B} = \frac{2}{A}\sum_i w_i, \qquad \hat{\phi}_s = \frac{2}{A}\sum_i \frac{w_i}{|\mathbf{\Omega}_i \cdot \mathbf{n}|}. \qquad (11b)$$

While solving:

$$\mathbf{\Omega} \cdot
abla \psi + \sigma_t \psi = rac{\sigma_s}{4\pi} \varphi + q \,,$$
(12a)

$$\psi(\mathbf{x}, \mathbf{\Omega}) = \psi_{\mathsf{inc}}(\mathbf{x}, \mathbf{\Omega}), \quad \mathbf{x} \in \partial \mathcal{D} \text{ and } \mathbf{\Omega} \cdot \mathbf{n} < 0.$$
 (12b)





Using MC allows us to move fixed sources out of the iteration.

1:
$$\hat{\phi}^{(0)}, \hat{\mathbf{T}}^{(0)}, \hat{\beta}^{(0)} \leftarrow \operatorname{mc}(q, \psi_{\operatorname{inc}})$$

2: $i \leftarrow 1$
3: while not converged $(\hat{\phi}^{(i-1)}, \hat{\phi}^{(i)})$ do
4: $\varphi^{(i)} \leftarrow \operatorname{sm}(Q_0, Q_1, \hat{\mathbf{T}}^{(i-1)}, \hat{\beta}^{(i-1)})$
5: $\hat{\phi}_{\operatorname{temp}}, \hat{\mathbf{T}}_{\operatorname{temp}}, \hat{\beta}_{\operatorname{temp}} \leftarrow \operatorname{mc}(\varphi^{(i)})$
6: $\hat{\phi}^{(i)} \leftarrow \hat{\phi}^{(0)} + \hat{\phi}_{\operatorname{temp}}$
7: $\hat{\mathbf{T}}^{(i)} \leftarrow \hat{\mathbf{T}}^{(0)} + \hat{\mathbf{T}}_{\operatorname{temp}}$
8: $\hat{\beta}^{(i)} \leftarrow \hat{\beta}^{(0)} + \hat{\beta}_{\operatorname{temp}}$
9: $i \leftarrow i + 1$
10: end while
11: return $\hat{\phi}^{(i)}$

 \triangleright Sample the fixed sources q and $\psi_{\rm inc}$

$$\triangleright$$
 Sample the variable source $\frac{\sigma_s}{4\pi}\varphi^{(i)}$



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The HSM error surface height is lowest in the north-east.



The HSM error is: $O(h) + O(N^{-1/2})$



We verified HSM using the Method of Manufactured Solutions.

$$\psi_{\mathsf{MMS}}(\mathbf{x}, \mathbf{\Omega}) = \frac{1}{4\pi} \Big(\sin(\pi x) \sin(\pi y) + \mathbf{\Omega}_x \mathbf{\Omega}_y \sin(2\pi x) \sin(2\pi y) \\ + \mathbf{\Omega}_x^2 \sin\left(\frac{5\pi}{2}x + \frac{\pi}{4}\right) \sin\left(\frac{5\pi}{2}y + \frac{\pi}{4}\right) + 0.5 \Big), \quad (13a)$$

$$\phi_{\mathsf{MMS}}(\mathbf{x}) = \int_{\mathbb{S}^2} \psi_{\mathsf{MMS}}(\mathbf{x}, \mathbf{\Omega}) \,\mathrm{d}\Omega\,, \tag{13b}$$

$$\bar{\phi}_{\mathsf{MMS}}(x_1, x_2, y_1, y_2) = \frac{1}{((x_2 - x_1)(y_2 - y_1))} \int_{x_1}^{x_2} \int_{y_1}^{y_2} \phi_{\mathsf{MMS}}(\mathbf{x}) \, \mathrm{d}y \, \mathrm{d}x \,. \tag{13c}$$





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The MMS solution that we seek with HSM is a histogram.







We observed the hypothesized error for the MMS problem.







HSM is faster than unaccelerated MC (UMC) in the TDL.



Thick Diffusion Limit (TDL):

$$\sigma_t o \sigma_t / \epsilon \,,$$
 (14a)

$$\sigma_a \to \epsilon \sigma_a \,, \tag{14b}$$

$$\sigma_s = \sigma_t - \sigma_a \,, \tag{14c}$$

$$q \to \epsilon q \,, \tag{14d}$$

for the TDL parameter $\epsilon \in (0,1],$ and let:

$$\epsilon \to 0$$
. (14e)





The Crooked Pipe is commonly used for comparing TRT methods.







The horizontal symmetry of CP allows top/bottom plots.







HSM is much more noisy than unaccelerated Monte Carlo.







The HSM variance is very large in the Thick Diffusion Limit.



$$\operatorname{Var}[\hat{\phi}] \approx \frac{1}{600} \sum_{i=1}^{600} (\hat{\phi}_i - \Phi)^2,$$
 (15)

where Φ is the mean estimate defined by,

$$\Phi = \frac{1}{600} \sum_{i=1}^{600} \hat{\phi}_i \,. \tag{16}$$





The rest of this talk is about variance reduction.

Motivation

Prior Work

Hybrid Second Moment Method

Deterministic Component of HSM

Monte Carlo Component of HSM

Numerical Results

Method of Manufactured Solutions Verification

Noisy Crooked Pipe

Variance Reduction

Difference Formulation

Incorrect Crooked Pipe

Generalized Difference Formulation

Correct Crooked Pipe

Conclusion







Compute the deviation of the intensity from isotropy.

Substitute $\psi = \frac{\varphi}{4\pi} + \tilde{\psi}$ into:

$$\mathbf{\Omega} \cdot
abla \psi + \sigma_t \psi = rac{\sigma_s}{4\pi} \varphi + q \,,$$
(17a)

$$\psi(\mathbf{x}, \mathbf{\Omega}) = \psi_{\mathsf{inc}}(\mathbf{x}, \mathbf{\Omega}), \quad \mathbf{x} \in \partial \mathcal{D} \text{ and } \mathbf{\Omega} \cdot \mathbf{n} < 0.$$
 (17b)

to get,

$$\mathbf{\Omega} \cdot \nabla \tilde{\psi} + \sigma_t \tilde{\psi} = -\frac{1}{4\pi} (\sigma_a \varphi + \mathbf{\Omega} \cdot \nabla \varphi) + q \,, \tag{18a}$$

$$\tilde{\psi}(\mathbf{x}, \mathbf{\Omega}) = \psi_{\mathsf{inc}}(\mathbf{x}, \mathbf{\Omega}) - \frac{\varphi(\mathbf{x})}{4\pi}, \quad \mathbf{x} \in \partial \mathcal{D} \text{ and } \mathbf{\Omega} \cdot \mathbf{n} < 0.$$
 (18b)





	Fixed	Variable		
Volume	q	$rac{\sigma_s}{4\pi} arphi$	$O(\epsilon)$	$O(1/\epsilon)$
Boundary	ψ_{inc}	0	O(1)	N/A
Volume	q	$-rac{1}{4\pi}(\sigma_a arphi + oldsymbol{\Omega} \cdot abla arphi)$	$O(\epsilon)$	O(1)
Boundary	$\psi_{\sf inc}$	$-rac{arphi}{4\pi}$	O(1)	O(1)





The new variance $\operatorname{Var}[\hat{\phi}_{\mathsf{new}}]$ is $\ll \operatorname{Var}[\hat{\phi}]$ in the TDL ($\epsilon \ll \epsilon^{-1}$).







The new solution is incorrect on material interfaces.







Modify the approach by replacing φ with $\bar{\varphi}$.

Before, we substituted $\psi=\frac{\varphi}{4\pi}+\tilde{\psi}$ to get:

$$\mathbf{\Omega} \cdot \nabla \tilde{\psi} + \sigma_t \tilde{\psi} = -\frac{1}{4\pi} (\sigma_a \varphi + \mathbf{\Omega} \cdot \nabla \varphi) + q \,, \tag{19a}$$

$$\tilde{\psi}(\mathbf{x}, \mathbf{\Omega}) = \psi_{\mathsf{inc}}(\mathbf{x}, \mathbf{\Omega}) - \frac{\varphi(\mathbf{x})}{4\pi}, \quad \mathbf{x} \in \partial \mathcal{D} \text{ and } \mathbf{\Omega} \cdot \mathbf{n} < 0.$$
 (19b)

Now, substitute $\psi = \frac{\bar{\varphi}}{4\pi} + \tilde{\psi}$ to get: $\mathbf{\Omega} \cdot \nabla \tilde{\psi} + \sigma_t \tilde{\psi} = \frac{\sigma_t}{4\pi} (\varphi - \bar{\varphi}) - \frac{1}{4\pi} (\sigma_a \varphi + \mathbf{\Omega} \cdot \nabla \bar{\varphi}) + q$, (20a) $\tilde{\psi}(\mathbf{x}, \mathbf{\Omega}) = \psi_{\text{inc}}(\mathbf{x}, \mathbf{\Omega}) - \frac{\bar{\varphi}(\mathbf{x})}{4\pi}$, $\mathbf{x} \in \partial \mathcal{D}$ and $\mathbf{\Omega} \cdot \mathbf{n} < 0$. (20b)





Choose $\bar{\varphi}$ such that $\nabla \bar{\varphi}$ is well-defined and $\varphi - \bar{\varphi}$ is $O(1/\sigma_t)$.

	Fixed	Variable		
Volume	q	$rac{\sigma_s}{4\pi}arphi$	$O(\epsilon)$	$O(1/\epsilon)$
Boundary	ψ_{inc}	0	O(1)	N/A
Volume	q	$-rac{1}{4\pi}(\sigma_a arphi + oldsymbol{\Omega} \cdot abla arphi)$	$O(\epsilon)$	O(1)
Boundary	ψ_{inc}	$-rac{arphi}{4\pi}$	O(1)	O(1)
Volume	q	$rac{\sigma_t}{4\pi}(arphi-ar{arphi})-rac{1}{4\pi}(\sigma_aarphi+oldsymbol{\Omega}\cdot ablaar{arphi})$	$O(\epsilon)$	O(?)
Boundary	ψ_{inc}	$-rac{ar{arphi}}{4\pi}$	O(1)	O(1)





Solve a transient heat conduction equation for $\bar{\varphi}$.

$$\frac{\partial \bar{\varphi}}{\partial t} = \nabla \cdot \frac{1}{\sigma_t} \nabla \bar{\varphi}, \quad \mathbf{x} \in \mathcal{D}, \qquad (21a)$$

$$\bar{\varphi}(\mathbf{x},0) = \varphi(\mathbf{x}), \quad \mathbf{x} \in \mathcal{D},$$

$$\bar{\varphi}(\mathbf{x},t) = \varphi(\mathbf{x}), \quad \mathbf{x} \in \partial \mathcal{D}.$$
(21b)
(21c)

Take one small timestep such that,

$$\frac{\Delta t}{h^2} \frac{1}{\max_{\mathbf{x}} \sigma_t} \ll 1.$$
(22)





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Find $\bar{\varphi} \in Y_p$ such that,

$$\frac{\partial}{\partial t} \int u \,\bar{\varphi} \,\mathrm{d}x - \int_{\Gamma_b} u \left(\frac{1}{\sigma_t} \nabla \bar{\varphi}\right) \cdot \mathbf{n} \,\mathrm{d}s + \int \nabla u \cdot \frac{1}{\sigma_t} \nabla \bar{\varphi} \,\mathrm{d}\mathbf{x}
- \int_{\Gamma_0} \left\{\!\!\left\{\frac{1}{\sigma_t} \nabla \bar{\varphi} \cdot \mathbf{n}\right\}\!\!\right\} \left[\!\left[u\right]\!\right] \,\mathrm{d}s + \sigma \int_{\Gamma_0} \left[\!\left[\bar{\varphi}\right]\!\right] \left\{\!\!\left\{\frac{1}{\sigma_t} \nabla u \cdot \mathbf{n}\right\}\!\!\right\} \,\mathrm{d}s =
- \sigma \int_{\Gamma_b} \varphi \left(\frac{1}{\sigma_t} \nabla u \cdot \mathbf{n}\right) \,\mathrm{d}s - k \int_{\Gamma_b} \left\{\!\!\left\{\frac{1}{h} \frac{1}{\sigma_t}\right\}\!\!\right\} \varphi u \,\mathrm{d}s \,, \quad \forall u \in Y_p \,. \tag{23}$$





Let Φ contain L^2 dofs for $\bar{\varphi}$. Then,

$$M\frac{\mathrm{d}\Phi}{\mathrm{d}t} = -K\Phi + f.$$
⁽²⁴⁾

Backward Euler is,

$$M\frac{\Phi^{n+1} - \Phi^n}{\Delta t} = -K\Phi^{n+1} + f.$$
 (25)

Thus,

$$(M + \Delta t K)\Phi^{n+1} = M\Phi^n + \Delta t f.$$
(26)

Define parameter α such that,

$$\Delta t = \alpha h^2 \left(\max_{\mathbf{x}} \sigma_t \right) \,. \tag{27}$$





The solution on material interfaces is no longer incorrect.







The generalized variance reduction fixes the noise issue.











	Runtime	Variance	FOM
HSM	0m 22s	$3.66\cdot 10^{-4}$	<mark>124.2</mark>
UMC	41m 35s	$5.20\cdot 10^{-5}$	7.7





Could HSM be competitive with IMD or DDMC?

	HSM	DDMC
Orders of magnitude speedups	\checkmark	\checkmark
No diffusion approximation	\checkmark	×
No phase-space partitioning	\checkmark	×
No issues with unstructured meshes	\checkmark	×
No iteration	\times	\checkmark
No linear solver	\times	\checkmark
No difference formulation	\times	\checkmark
Demonstrated in production calculations	\times	\checkmark



Conclusion: the HSM method described in this talk seems useful.

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The future work for HSM is a path to production calculations.

- 1. time dependence, $\psi(\mathbf{x}, \mathbf{\Omega}, t)$
- 2. frequency dependence, $\psi(\mathbf{x}, \mathbf{\Omega}, t, \nu)$
- 3. 1D Spherical, 2D RZ, and 3D
- 4. hydrodynamics coupling
- 5. physical scattering
- 6. graphics processors
- 7. spectral line transport
- 8. high order

Progress Porting LLNL Monte Carlo Transport Codes to the AMD Instict MI300A APU at 1:25 PM today in Special Session on GPU Computing



llnl.gov/article/52336/llnl-dedicates-el-capitan-ushering-new-era-

supercomputing-national-security



Only 8% of the HSM runtime is in the deterministic component.







defaults="

runvars.convergence_criterion = 0.001; runvars.num_bdr_src_particles = 16e6; runvars.num_vol_src_particles = 16e6; runvars.mesh = [[lcp5.mesh]]; runvars.output_root_filename = "

srun -n112 ./hyr lcp.lua -e "\$defaults [[hsm_lcp_16e6_16e6]]"

Running lcp5.mesh-16000000-16000000 (mesh-np) The total weight is 0.50005 The total weight is -1.50598 Cycle 1: Maxres 0.00e+00 0.00e+00 Runtime 8.96e-01 4.78e+00 The total weight is -1.24976 Cycle 2: Maxres 4.41e-01 3.04e-01 Runtime 1.08e-01 2.49e+00 The total weight is -1.15745 Cycle 3: Maxres 2.13e-01 7.89e-02 Runtime 2.30e-01 8.06e-01 The total weight is -1.12240 Cycle 4: Maxres 9.70e-02 2.81e-02 Runtime 9.56e-02 8.10e-01 The total weight is -1.10688 Cycle 5: Maxres 3.88e-02 1.14e-02 Runtime 9.18e-02 8.07e-01 The total weight is -1.09918 Cycle 6: Maxres 1.71e-02 4.97e-03 Runtime 1.58e-01 8.26e-01 The total weight is -1.09509 Cycle 7: Maxres 8.47e-03 2.26e-03 Runtime 1.47e-01 8.03e-01 The total weight is -1.09284 Cycle 8: Maxres 4.21e-03 1.06e-03 Runtime 1.53e-01 8.16e-01 The total weight is -1.09158 Cycle 9: Maxres 2.11e-03 5.06e-04 Runtime 1.36e-01 8.08e-01 The total weight is -1.09085 Cycle 10: Maxres 1.06e-03 2.48e-04 Runtime 1.39e-01 8.06e-01 The total weight is -1.09044 Cycle 11: Maxres 5.31e-04 1.24e-04 Runtime 2.37e-01 8.11e-01



Resetting the PRNG seed makes the HSM iteration converge.







We sample volume sources uniformly.

$$\lim_{N \to \infty} \sum_{i=1}^{N} w_i = \int_{\mathcal{D}} \int_{\mathbb{S}^2} q \, \mathrm{d}\Omega \, \mathrm{d}\mathbf{x} \,, \tag{28a}$$
$$\int_{\mathcal{D}} \int_{\mathbb{S}^2} q \, \mathrm{d}\Omega \, \mathrm{d}\mathbf{x} \approx \frac{V}{N} \sum_{i=1}^{N} q(\mathbf{x}_i, \mathbf{\Omega}_i) \,, \tag{28b}$$
$$W = \int_{\mathcal{D}} \int_{\mathbb{S}^2} \mathrm{d}\Omega \, \mathrm{d}\mathbf{x} \,, \qquad \mathbf{x}_i = U(\mathcal{D}) \,, \qquad \mathbf{\Omega}_i = U(\mathbb{S}^2) \,. \tag{28c}$$





We sample boundary sources uniformly.

$$\lim_{M \to \infty} \sum_{i=1}^{M} w_i = \int_{\partial \mathcal{D}} \int_{\mathbf{\Omega} \cdot \mathbf{n} < 0} |\mathbf{\Omega} \cdot \mathbf{n}| \psi_{\mathsf{inc}} \, \mathrm{d}\Omega \, \mathrm{d}\mathbf{x} \,, \tag{29a}$$

$$\int_{\partial \mathcal{D}} \int_{\mathbf{\Omega} \cdot \mathbf{n} < 0} |\mathbf{\Omega} \cdot \mathbf{n}| \psi_{\mathsf{inc}} \, \mathrm{d}\Omega \, \mathrm{d}\mathbf{x} \approx \frac{S}{M} \sum_{i=1}^{M} |\mathbf{\Omega}_{i} \cdot \mathbf{n}| \psi_{\mathsf{inc}}(\mathbf{x}_{i}, \mathbf{\Omega}_{i}), \qquad (29b)$$

$$S = \int_{\partial \mathcal{D}} \int_{\mathbf{\Omega} \cdot \mathbf{n} < 0} \mathrm{d}\Omega \,\mathrm{d}\mathbf{x} \,, \qquad \mathbf{x}_i = U(\partial \mathcal{D}) \,, \qquad \mathbf{\Omega}_i = U(\mathbb{S}_h) \,. \tag{29c}$$





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The iteration converges when the relative difference of successive iterates falls below a user-provided threshold, η .

$$\max_{j} \left(\frac{|\hat{\phi}_{j}^{(i-1)} - \hat{\phi}_{j}^{(i)}|}{\hat{\phi}_{j}^{(i-1)}} \right) < \eta, \qquad j = 1, \dots, |\mathcal{T}|,$$
(30)





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The error in the two scaling studies is computed differently

Element scaling study error
$$=rac{||\hat{\phi}-ar{\phi}||_2}{|\mathcal{T}|}\,,$$
 (31a)

Particle scaling study error
$$= ||\hat{\phi} - \bar{\phi}||_2$$
. (31b)




Our code is only 5500 lines, not including dependencies.

Lines of code	Filename			
20	wkt_conduction.h wkt_mmsvars.h system.c eval.c wkt_sources.h wkt_runvars.h write.c hyr.c psmm.cpp	- <u> </u>	/ersion	Library
22			1.14.3	hdf5
20 37			2.33.0	hypre
39			1.0.0	irep
57			5.4.0 5.1.0	nua metis
481			4.6	mfem
1621			4.40.3	parmeti
2463	mc.c		5.3.0	superlu
5512	total			





The UMC variance is highest in the optically-thick material.







The HSM variance is highest at the inflow boundary.







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